



# Fouling mitigation and cleanability of TiO<sub>2</sub> photocatalyst-modified PVDF membranes during ultrafiltration of model oily wastewater with different salt contents

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Received: 15 August 2017 / Accepted: 10 December 2017  
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## Abstract

In the present study, TiO<sub>2</sub>-coated ultrafiltration membranes were prepared and used for oily water filtration (droplet size < 2 µm). The aim of this work was to investigate the effect of different salt contents on fouling and filtration properties of neat and TiO<sub>2</sub>-coated membranes during oil-in-water emulsion filtration. The effect of the TiO<sub>2</sub> coating on the flux, surface free energy, and retention values was measured and compared with the neat membrane values. The cleanability of the fouled TiO<sub>2</sub>-coated membranes by UV irradiation was also investigated by measuring flux recovery and contact angles, and the chemical changes during cleaning were characterized by ATR-IR. It was found that increasing the salt content of the model wastewaters, oil-in-water emulsions, increased the zeta potential and the size of the droplets. The presence of the TiO<sub>2</sub> coating decreases the membrane fouling during oily emulsion filtration compared to the neat membrane, due to the hydrophilicity of the coating regardless of the salt content of the emulsions. The neat and coated membrane oil retention was similar, 96 ± 2%. The coated membrane can be effectively cleaned with UV irradiation without additional chemicals and a significant flux recovery can be achieved. Monitoring of the cleaning process by following the membrane surface wettability and ATR-IR measurements showed that the recovery of flux does not mean the total elimination of the oil layer from the membrane surface.

**Keywords** TiO<sub>2</sub>-coated membrane · PVDF · Salt content · Oil-in-water emulsion · Ultrafiltration · Fouling

## Introduction

Waste thermal waters used for greenhouse heating often contain considerable amounts of oily impurities forming oil-in-water emulsions with additional dissolved organics and different amounts of dissolved salts. Stabilized oil droplets (< 10 µm) cannot be removed from emulsions by conventional water treatment techniques, but membrane filtration may be suitable to overcome this shortcoming (Fakhru'l-Razi et al. 2009; Dickhout et al. 2017). Oil-containing industrial wastewaters may vary significantly in their salt content: in case of produced waters from a few parts per million (ppm) up to about 300,000 mg L<sup>-1</sup> (Fakhru'l-Razi et al. 2009).

Ultrafiltration is an efficient method to treat these oil-in-water emulsions, without chemical additives and low energy cost compared to traditional separation methods (He and Jiang 2008; Kiss et al. 2013). Polymer membranes are the most commonly used type of membranes in water and wastewater treatment due to their low price and easy maintenance, but the main problem to be solved is fouling mitigation during membrane filtration processes. An appropriate fouling mitigation method could be to increase membrane hydrophilicity by modifying membranes with TiO<sub>2</sub> nanoparticles (Leong et al. 2014; Bai et al. 2010; Molinari et al. 2002). Photocatalyst-modified membranes proved to have good fouling mitigating properties in case of activated sludge filtration (Bae and Tak 2005) and photocatalytic bactericidal properties (Kim et al. 2003) and showed significant photocatalytic activity in case of model pollutants like methylene blue, humic acid, and 4-nitrophenol (Bai et al. 2010; Molinari et al. 2002). To our best knowledge, the feasibility of photocatalyst-modified membranes to treat real oil-in-water emulsions with high salt content has not been investigated. The emulsion properties (e.g., droplet size, ionic strength, temperature, pH, emulsifier

Responsible editor: Philippe Garrigues

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concentration, and the volume ratio of oil to water phase) determine the interfacial interactions between the membrane surface and the emulsion and thus the fouling propensity of the membrane; in order to minimize fouling, better understanding of these effects is necessary (Fakhru'l-Razi et al. 2009; Dickhout et al. 2017).

For membrane coating and modification,  $\text{TiO}_2$  is an appropriate photocatalyst due to its good physical and chemical properties, availability, high photocatalytic activity, and desirable hydrophilic properties (Bet-moushoul et al. 2016; Molinari et al. 2016; Yi et al. 2011; Hu and Scott 2008; Leong et al. 2014). The membrane material to be suitable for modification with  $\text{TiO}_2$  must be resistant to UV irradiation and to the reactive species generated during the photocatalytic reaction (Bellobono et al. 2005; Chin et al. 2006); properties of PVDF membranes meet these requirements (Chin et al. 2006).

Fouling occurs when materials of colloidal size (with dimensions  $< 1 \mu\text{m}$ ) are adsorbed on solid surfaces, which is determined by interactions between colloidal particles and membrane surface, which can develop, due to generally attractive van der Waals interactions, and generally repulsive electrostatic double-layer forces, due to the surface charges of the membrane and the colloidal particles. This DLVO theory can be extended by integrating the hydrophobic interactions taking into consideration the surface free energy of polar interactions. The net effect is a balance between all possible interactions (Oliveira 1997). Interactions of colloidal particles with polymeric membrane surfaces are influenced by membrane surface morphology (roughness). Earlier works (Hoek et al. 2003) show that the repulsive interaction energy barrier between a colloidal particle and a rough membrane is lower than the corresponding barrier for a smooth membrane, and it was suggested that the valleys created by the membrane surface roughness produce wells of low interaction energy in which colloidal particles may preferentially deposit, increasing the fouling. However, larger particles are not able to adhere, because gravitational and hydrodynamic forces are strong enough to remove them from the “peaks” of the rough surface—in this case, the fouling is decreasing with increased surface roughness (Oliveira 1997), which may occur by covering the surface with  $\text{TiO}_2$ . It should be clarified what is the resultant effect of the contradicting changes of the  $\text{TiO}_2$ -modified surface properties (increased hydrophilicity and increased roughness) (Kovács et al. 2017) on fouling propensity.

The aim of this work was to prepare  $\text{TiO}_2$ -coated PVDF membranes to be applicable for cleaning by heterogeneous photocatalysis after filtration of model oily wastewater containing 100 ppm crude oil and different salt concentrations. As oil-containing industrial wastewaters may vary significantly in their salt content, examined salt concentrations were chosen to cover three orders of magnitude from 250 to 25,000  $\text{mg L}^{-1}$ . The effect of salt concentration on fouling and on filtration properties of neat and  $\text{TiO}_2$ -coated membranes during oil-in-water emulsion

filtration was investigated. Furthermore, the cleanability of the fouled  $\text{TiO}_2$ -coated membranes by UV irradiation was investigated by monitoring the physical and chemical changes of the foulants on the membrane surface.

## Materials and methods

### Membrane and catalyst characteristics

Poly(vinylidene fluoride) membranes (PVDF 200 (New Logic Research Inc., USA)) with a 250-kDa molecular weight cutoff (MWCO) were coated with commercial  $\text{TiO}_2$  Aeroxide P25 (Evonic Industries). Commercial Aeroxide P25 titanium dioxide has spherical shape with a primer particle size of  $\sim 25 \text{ nm}$  (Veréb et al. 2012); however, it should be noted that in a suspension, it forms aggregates nearly  $1 \mu\text{m}$  in diameter (Mogyorósi et al. 2010). This titania is a mixture of anatase (90%) and rutile (10%) phase, and it has a specific surface area of  $49 \text{ m}^2 \text{ g}^{-1}$ .

### Oil-in-water emulsions

The model wastewater (oil-in-water emulsion,  $c_{\text{oil}} = 100 \text{ ppm}$ ) was prepared from crude oil (Algyő-area, Hungary) and Milli-Q water (with no added salt, with 250, 2500, and 25,000  $\text{mg L}^{-1}$  salt, respectively) by ultrasonication. The composition of the added salts and their mass ratios are given in Table 1. The pH of the oil-in-water emulsions with no added salt, with 250, 2500, and 25,000  $\text{mg L}^{-1}$  salt, was 6.9, 8.5, 8.6, and 8.4, respectively. The 2500- $\text{mg L}^{-1}$  composition of the model water represents an underground water composition characteristic in the southern part of the Great Hungarian Plain (Table 1).

The emulsion was prepared in two steps using crude oil (Algyő, Hungary) and distilled water. In the first step, 1 wt% emulsion was prepared by intensive stirring (35,000 rpm), then 5 mL of this emulsion was inoculated into 495 mL of distilled water (or the water with added salt content) directly below the transducer of an ultrasonic homogenizer (Hielscher UP200S) resulting in stable oil-in-water emulsion ( $c_{\text{oil}} = 100 \text{ ppm}$ ). The duration of homogenization was 10 min, maximal amplitude and cycle were applied, and the emulsion was thermostated to  $25^\circ\text{C}$ .

### Membrane coating and filtration

The membrane preparation was carried out according to the method developed and described in our earlier work (Kovács et al. 2017): 100 mL of  $0.4 \text{ g L}^{-1}$  catalyst suspension was filtered through the membrane in a dead-end cell, at 0.1 MPa without stirring, at  $20^\circ\text{C}$ . It results in  $1.2 \text{ mg cm}^{-2}$   $\text{TiO}_2$  coating that fully covers the membrane surface and

**Table 1** Salt content and ratio of the model wastewaters

Salt content	wt%
NaHCO <sub>3</sub>	91.61
NH <sub>4</sub> Cl	2.17
FeCl <sub>3</sub>	0.11
CaCl <sub>2</sub>	0.77
MgSO <sub>4</sub>	0.67
KCl	0.84
NaCl	3.79

forms a stable layer under operational conditions (Kovács et al. 2017). The filtration was carried out with a Millipore batch filtration unit (XFUF04701, Solvent-resistant Stirred Ultrafiltration Cell, Millipore, USA); after filtration, the membranes were removed from the cell, gently rinsed with distilled water, and kept wet until used.

The filtrations of the model solution were carried out at 0.3 MPa transmembrane pressure with 50 rpm stirring at 20 °C. Before every experiment, the membranes were immersed in water overnight and 1 L water was filtered through them to achieve a constant flux. The flux of the neat membrane was  $820 \pm 30 \text{ L m}^{-2} \text{ h}^{-1}$ . Relative fluxes are shown in the following that are all in proportion to this value. In each filtration experiment, 250 mL water or model solution was filtered to volume reduction ratio (VVR) 5. VRR [–] was defined as:

$$\text{VRR} = \text{VF}/(\text{VF}-\text{VP}) \quad (1)$$

where VF and VP are the volume of the feed and permeate ( $\text{m}^3$ ) respectively at any time.

The UV cleaning of the fouled membranes was carried out in the filtration unit using a modified cap so that the UV light source could be fitted in it (Kovács et al. 2017). The UV light source was a mercury-vapor lamp, 40 W,  $\lambda = 254 \text{ nm}$  (Germipak LightTech, Hungary). The UV irradiation of the fouled membranes lasted from 1 up to 6 h. Before and after each hour of irradiation, the membrane surface was rinsed with water, water flux measurements were carried out, parallel membranes were dried, and contact angles were measured. In the modified cell, 100 mL distilled water was over the membranes during UV irradiation, which was changed in every hour.

## Analytical methods and calculations

pH of the emulsions was measured by a Consort C535 type multimeter. The size distribution and zeta potentials were determined by dynamic light scattering measurements using a Malvern ZetaSizer4 type equipment.

Determination of the chemical oxygen demand (COD) was based on the standard potassium-dichromate oxidation

method; for the analysis, standard test tubes (Lovibond) were used. The digestions were carried out in a COD digester (Lovibond, ET 108) for 2 h at 150 °C; the COD values were measured with a COD photometer (Lovibond PC-CheckIt).

Membrane hydrophilicity was quantified by measuring the contact angle that was formed between the (neat and coated) dry membrane surface and distilled water. Ten microliters of distilled water was carefully dropped onto the membrane surface and immediately measured. Contact angles were measured using the sessile drop method (Dataphysics Contact Angle System OCA15Pro, Germany). The same steps were taken to measure the glycerol and the three different wastewater contact angles. Every measurement was repeated five times, and the average values were calculated and are presented in this work. The surface free energies of membranes were calculated by the Owens, Wendt, Rabel, and Kaelble (OWRK) method, using the OCA15 SCA21 software package (Dataphysics).

The neat, TiO<sub>2</sub>-coated, fouled, and UV-cleaned membrane surfaces were also characterized by ATR-IR (attenuated total reflectance). The spectra were recorded with a BIO-RAD Digilab Division FTS-65A/896 FT-IR (Fourier-transform infrared) spectrophotometer with  $4\text{-cm}^{-1}$  resolution. The  $4000\text{--}1000\text{-cm}^{-1}$  wavenumber range was investigated. Two hundred fifty-six scans were collected for each spectrum.

The retention (%) values were calculated by the following equation:

$$R = \left(1 - \frac{c}{c_0}\right) \cdot 100\% \quad (2)$$

where  $c$  is the average COD of the permeate phase and  $c_0$  is the COD of the feed.

The filtration resistances were determined according to the resistances in the series model, as membrane resistance ( $R_M$ ) was calculated as follows:

$$R_M = \frac{\Delta p}{J_W \eta_W} \quad [\text{m}^{-1}] \quad (3)$$

where  $\Delta p$  is the transmembrane pressure (Pa),  $J_W$  is the water flux of the clean membrane ( $\text{m}^3 \cdot \text{m}^{-2} \cdot \text{s}^{-1}$ ), and  $\eta_W$  is the viscosity of the water ( $\text{Pa} \cdot \text{s}$ ).

The irreversible resistance ( $R_{\text{Irrev}}$ ) was determined by measuring the water flux on the used membrane after the filtration, followed by a purification step (intensive rinsing with distilled water):

$$R_{\text{Irrev}} = \frac{\Delta p}{J_{WA} \eta_W} - R_M \quad [\text{m}^{-1}] \quad (4)$$

where  $J_{WA}$  is the water flux after the cleaning procedure.

The reversible resistance ( $R_{\text{Rev}}$ —caused by not adhered oil layer and concentration polarization layer) can be calculated as follows:

$$R_{\text{Rev}} = \frac{\Delta p}{J_c \eta_{\text{WW}}} - R_{\text{Irrev}} - R_{\text{M}} \quad [\text{m}^{-1}] \quad (5)$$

where  $J_c$  is the flux at the end of the filtration and  $\eta_{\text{WW}}$  is the viscosity of the emulsion. The total resistance ( $R_{\text{T}}$ ) can be calculated as follows:

$$R_{\text{T}} = R_{\text{M}} + R_{\text{Irrev}} + R_{\text{Rev}} \quad [\text{m}^{-1}] \quad (6)$$

## Results and discussion

### Characterization of the o/w emulsions with different salt contents

In this study, first the effects of the salt content on the oil droplet size and zeta potential were investigated to determine the characteristics of the different emulsions. The same emulsion production method resulted in four emulsions with different average droplet size, depending on the salt content, but in every case, the droplets were smaller than 2  $\mu\text{m}$ . With the increase of the salt content, the average droplet size (Fig. 1) and zeta potential increased (−30, −58, −60, and −15 mV, respectively), resulting in bigger droplets with increased negative surface charge except of the highest salt content. The increase in the droplet size and zeta potential may be the result of the too high cation concentration, suggesting that the ions do not take a part in zeta potential modification and can act as binders between the oil droplets (Yi et al. 2011; Hesampour et al.

2008). The zeta potential of crude oil droplets dispersed in saline water is dependent on the pH and ionic strength; the decrease in the magnitude of zeta potential of droplets is in accordance with other results (Kolltweit 2016; Mahani et al. 2015).

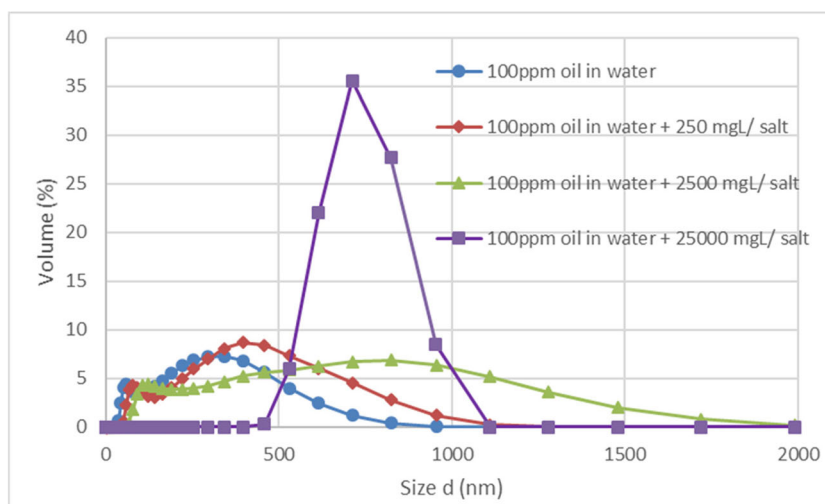
### Characterization of neat and $\text{TiO}_2$ -covered membrane surfaces

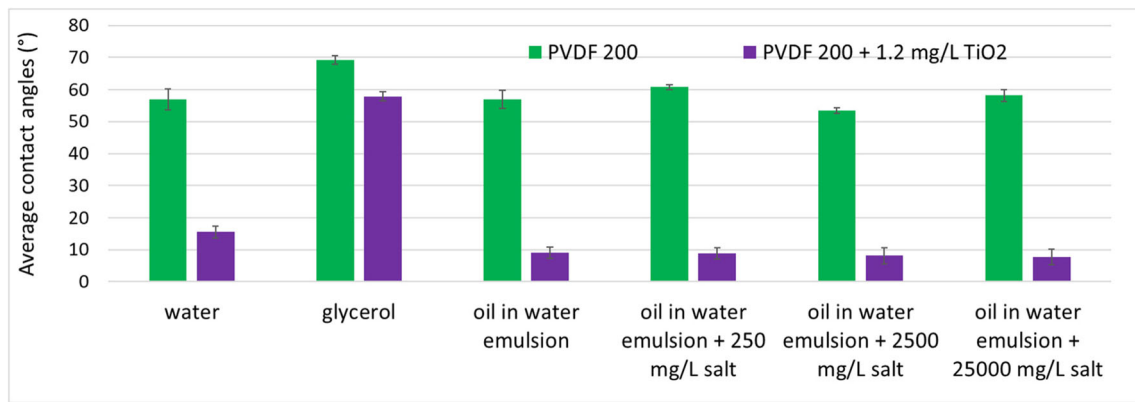
In order to characterize the neat and modified membrane surfaces, the wettability (Fig. 2) and surface free energy changes were measured. By coating the membrane with  $\text{TiO}_2$ , the surface free energy of the membrane increases from 30 to 48  $\text{m Nm}^{-1}$ . The oil-in-water emulsions with different salt contents had no significant difference between their contact angles.

### Membrane fouling

In the next series of experiments, the membrane resistances were investigated by means of the resistances-in-series method. It was found that  $\text{TiO}_2$  forms a dense hydrophilic layer on the membrane surface (Bai et al. 2010; Kovács et al. 2017) that slightly increases the membrane resistance (Fig. 3). The catalyst layer reduces both the reversible and irreversible resistances compared to the neat membrane. The interactions according to DLVO theory and hydrophobic interactions determine the wettability and the surface free energy. According to earlier studies, lowering the surface free energy (which means lower polar interactions) and increasing the hydrophilicity may improve the fouling resistance of a membrane (Razmjou et al. 2011; Low et al. 2015). In our case, it was found that although the  $\text{TiO}_2$  coating increased the surface free energy, but both reversible and irreversible fouling significantly decreased. This

**Fig. 1** Size distribution of oil droplets in emulsions with different (no added, 250, 2500, and 25,000  $\text{mg L}^{-1}$ ) salt contents





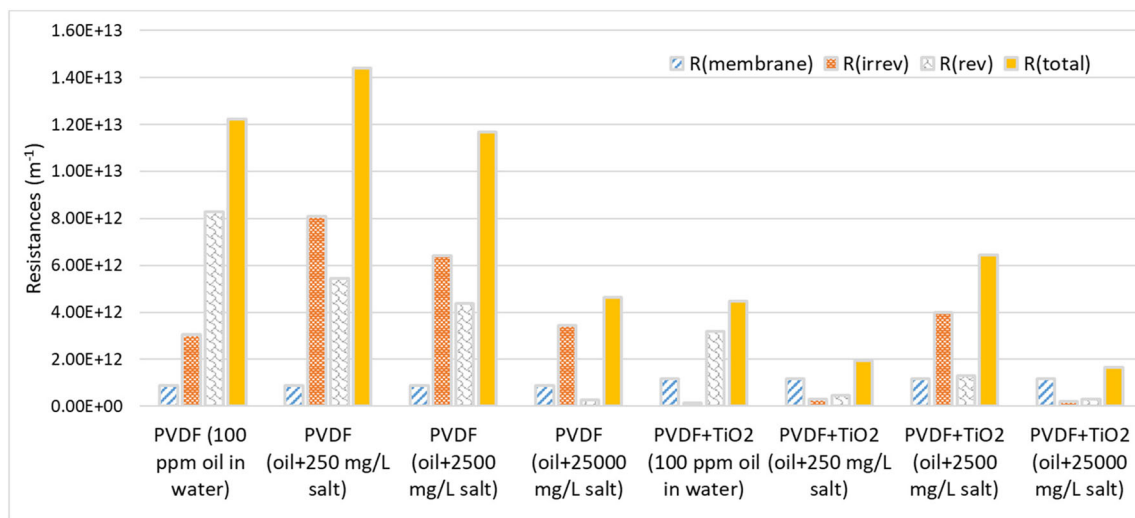
**Fig. 2** Water, glycerol, and the four model wastewater average contact angles of the neat and TiO<sub>2</sub>-coated PVDF 250-kDa membranes

means that the increased hydrophilicity (regarding to higher negative surface charge) of the surface leading to the repulsive electrostatic forces and/or the surface microroughness of the coating comes into prominence over the attractive van der Waals and hydrophobic interactions.

The effect of salt content on the filtration resistances was found to be contradictory; while in case of neat PVDF membrane, the salt content decreased the irreversible fouling, and in case of TiO<sub>2</sub>-covered surfaces, it was observed that the increased salt content increased the irreversible fouling. Although decreased fouling could be expected due to higher magnitude of the zeta potential of the emulsion at higher salt content, the slightly increased irreversible (non-washable) resistances can be explained by the DLVO theory, as increase in ionic strength lowers the energy barrier and hence favors adhesion (Ruckenstein and Kalthod 1981). In case of TiO<sub>2</sub>-covered surfaces, the lower salt concentration resulted in lower filtration resistances, probably due to increased surface zeta potential resulting in increased

repulsive electrostatic forces. Furthermore, at higher salt concentrations, the magnitude of zeta potential of the surface may be decreased, as earlier studies showed (Luxbacher et al. 2014; Salgın et al. 2013), leading to increased role of the attractive van der Waals interactions, and thus the adhesion.

In case of 25,000 mg L<sup>-1</sup> salt-containing oily water after the filtration by rinsing the fouled membrane surface with water, the TiO<sub>2</sub> coating washed off, together with the adsorbed oil layer causing lower filtration resistances. It means that high salt content may destabilizes the TiO<sub>2</sub> coating. This effect was then further examined at five different salt concentrations between 2500 and 25,000 mg L<sup>-1</sup> (at 7500, 10,000, 12,500, 15,000, and 120,000 mg L<sup>-1</sup>). In case of waters with salt contents higher than 12,500 mg L<sup>-1</sup>, the TiO<sub>2</sub> layer destabilizes and washes off the membrane surface. This is the reason why the membranes fouled by 25,000 mg L<sup>-1</sup> salt-containing oily waters were not included in further photocatalytic examinations.



**Fig. 3** Resistances of neat and TiO<sub>2</sub>-coated PVDF 250-kDa membranes during the four model wastewater filtrations

The neat and TiO<sub>2</sub>-coated membrane oil retention was similar,  $96 \pm 2\%$ .

### Cleanability of the fouled TiO<sub>2</sub>-coated membranes by UV irradiation

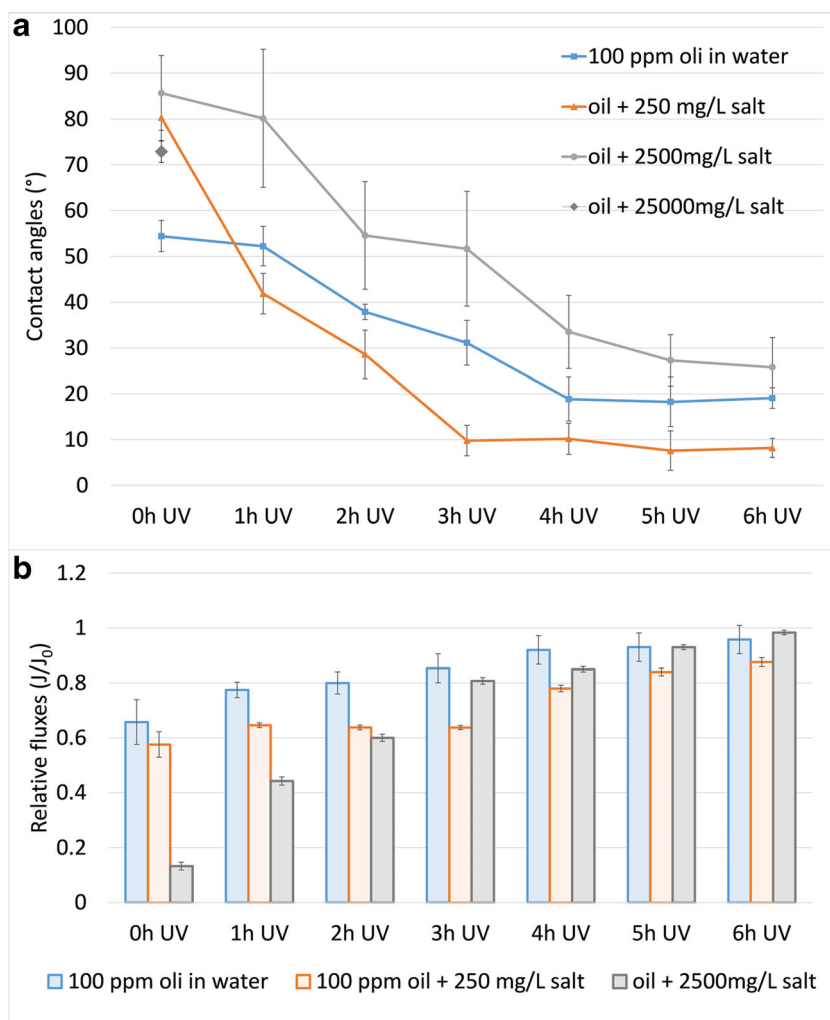
After oil-in-water emulsion filtration, the membrane cleanability by means of photocatalysis (without any additional chemicals) was investigated. The fouled membranes were taken out of the cell and rinsed with distilled water to remove the oil layer if possible. Then, the membranes were put back in the cell filled with 100 mL distilled water and irradiated with UV light for 6 h. The contact angle and water flux changes were measured after every step and hourly during the UV cleaning process. This cycle was repeated in every case. To examine the cleaning efficiency, relative water fluxes and contact angles of the fouled and cleaned surfaces were compared (Fig. 4). It was found that the oil remaining on the TiO<sub>2</sub>-coated membrane surface after filtration significantly increases the membrane surface hydrophobicity; the membrane surface

hydrophilicity is in accordance with the filtration resistances (see Figs. 3 and 4).

During UV irradiation, the surface hydrophilicity was increased, and nearly total flux recovery was achieved, showing that the fouled membranes can be effectively cleaned with UV irradiation. It also was observed that the relative flux recovery was the most effective in case of the 2500-mg L<sup>-1</sup> salt concentration. The efficiency of the heterogeneous photocatalysis is determined by several factors and these factors affect the degradation efficiency in a very complex way: besides the effect of water matrix (ionic strength, pH, inorganic salt content), the degradation is determined by the adsorption of the pollutants on the catalyst surface; in case of 2500 mg L<sup>-1</sup> salt concentration, more oil was adsorbed on the TiO<sub>2</sub> surface (according to the contact angle and filtration resistance results) which may have been more easily available for photocatalytic degradation.

At the same time, the contact angle values and the ATR-IR spectra (Figs. 4a and 6) show that the oil layer does not decompose entirely during 6 h irradiation, which may cause more extended fouling in case of reusing the membranes

**Fig. 4** Water contact angle (a) and relative water flux changes (b) of the three wastewater fouled 1.2-mg/cm<sup>2</sup> TiO<sub>2</sub>-coated membranes during UV cleaning



(Luján-Facundo et al. 2015). In case of the oil-in-water emulsion with added salt, a less uniform oil layer forms on the membrane surface during filtration. These layers during irradiation contrary to the oil layer with no added salt do not faint in color gradually with the irradiation time; they break off in pieces, which can be attributed to the coagulation effect of the  $\text{Ca}^{2+}$  and  $\text{Fe}^{3+}$  ions present (Ríos et al. 1998). This effect is also in accordance with the increasing droplet size of the emulsions with the increased salt content (Fig. 1).

### ATR-TIR measurements

At first, the spectra of neat and  $\text{TiO}_2$ -coated membranes were compared (Fig. 5). Typical absorption peaks of the PVDF membrane are at  $1402\text{ cm}^{-1}$  overlapping with,  $1382\text{ cm}^{-1}$  (bending vibration of  $-\text{CH}_2$ ),  $1210\text{ cm}^{-1}$  (wagging vibration of  $-\text{CH}_2$ ),  $1172\text{ cm}^{-1}$  (twisting vibration of  $-\text{CH}_2$ ), and  $1070\text{ cm}^{-1}$  (in plane wagging vibration of  $\text{C}-\text{F}$ ). The  $\text{TiO}_2$  coating also has the typical vibrations; the broad absorption band at around  $3600\text{--}2800\text{ cm}^{-1}$  is related to the stretching vibration modes of the  $\text{H}_2\text{O}$  molecules. The broad band contains not only the components of the  $\text{H}_2\text{O}$  molecules with different numbers of hydrogen bonds but also the Fermi resonance attributed to the overtone absorption of the bending mode  $\delta$  ( $\text{H}_2\text{O}$ ) at  $1637\text{ cm}^{-1}$  (Atitar et al. 2015). Comparing spectra, it can be stated that  $\text{TiO}_2$  covers the membrane surface, overlying the membrane's vibrations.

The crude oil layer on the surface can be characterized by pronounced signatures at  $2914$  and  $2850\text{ cm}^{-1}$  (CH stretching vibrations) and  $1460\text{--}1377\text{ cm}^{-1}$  (CH bending vibrations). During heterogeneous photocatalytic reactions, this spectra change: typical absorption peaks of  $-\text{CH}_2$  (at  $1400\text{ cm}^{-1}$  and  $1174\text{ cm}^{-1}$ ) can be observed instead of the characteristic peak of  $-\text{CH}_3$  at  $1460\text{ cm}^{-1}$  (Fig. 6). The bands near  $1200\text{ cm}^{-1}$  also could be assigned to the axial asymmetric stretching vibrations of the bonds pertaining to the  $\text{CC}(=\text{O})\text{-O}$  functional group; those bands near  $1170\text{ cm}^{-1}$  may correspond to the

axial asymmetric stretching vibrations of bonds' characteristic to the  $\text{O}-\text{C}-\text{C}$  ester group, but the absence of an absorption band corresponding to stretching vibrations of the carbonyl ( $\text{C}=\text{O}$ ) functional group in the region between  $1700$  and  $1800\text{ cm}^{-1}$  denotes that the oxidized by-products as small acids and aldehydes cannot remain adsorbed in the surface, as they might be water soluble and can be washed off by the rinsing after the UV irradiation. The presence of salt did not affect these characteristics; however, in case of  $2500\text{ mg L}^{-1}$  salt content, the oil layer covers the  $\text{TiO}_2$  surface (covering the water absorption band around  $1680\text{ cm}^{-1}$ ), in accordance with the observed increased fouling of the membrane. Even after 6 h of irradiation, the presence of the oil layer was detectable, despite that the contact angles returned or closely correlated to the initial value of the clean  $\text{TiO}_2$ -coated membrane.

### Conclusions

$\text{TiO}_2$ -coated poly(vinylidene fluoride) (250 kDa) ultrafiltration membranes were prepared using the physical deposition method by filtering  $\text{TiO}_2$  suspension through the membrane without stirring in order to be applicable for cleaning by heterogeneous photocatalysis after filtration of oily wastewater. Investigations were performed with oil-in-water emulsions with different salt contents. Characterization of emulsions shows that the droplet size and zeta potential of the droplets increase with increasing salt content.  $\text{TiO}_2$ -covered membranes were more hydrophilic than neat membranes, and according to ATR-IR measurements, the coverage was appropriate. During filtration, the  $\text{TiO}_2$  coating significantly decreased both reversible and irreversible filtration resistances due to increased hydrophilicity (regarding to higher negative surface charge) of the surface leading the repulsive electrostatic forces and/or the surface microroughness of the coating to come into prominence over the attractive van der Waals and hydrophobic interactions. With increasing salt content of the emulsion,

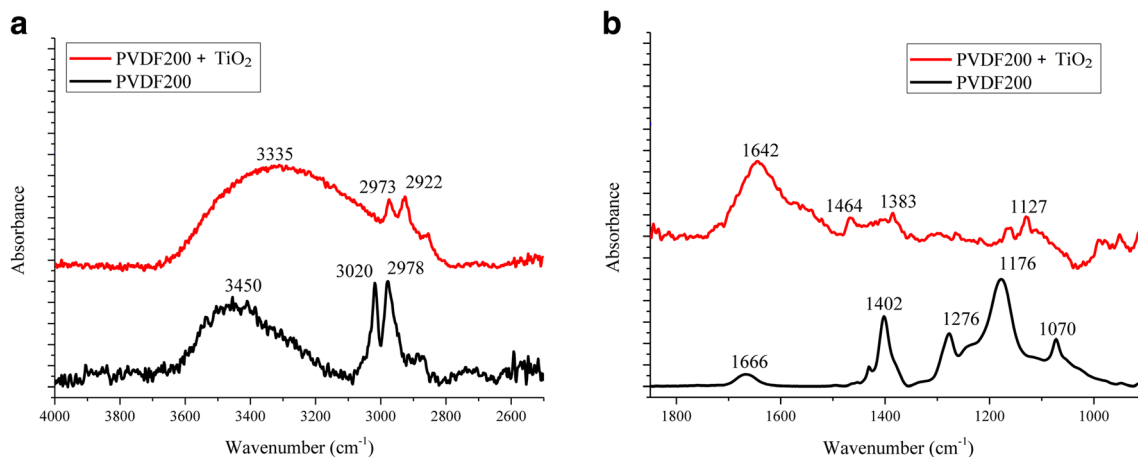
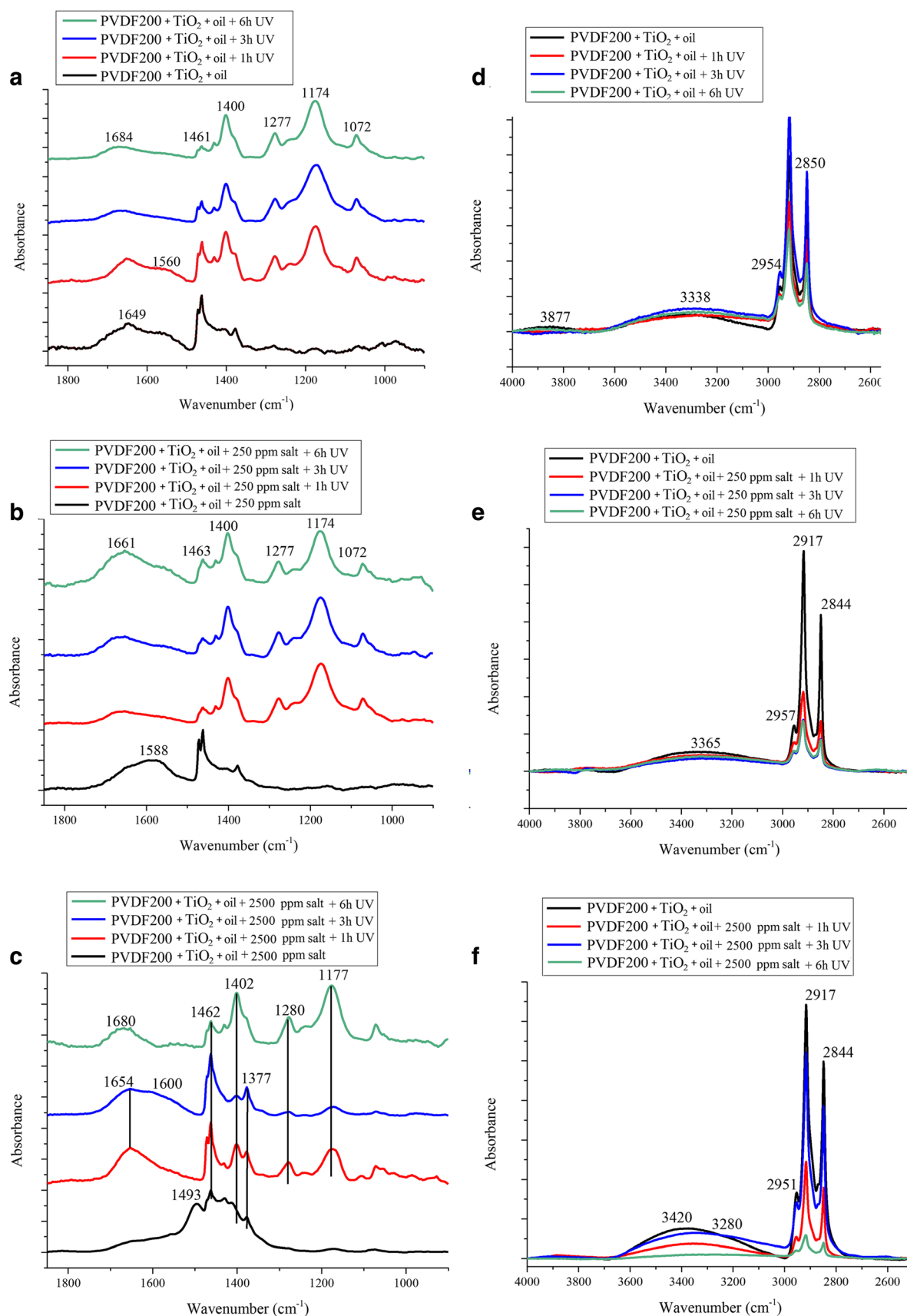


Fig. 5 ATR-IR spectra of neat and  $\text{TiO}_2$ -covered PVDF membranes



**Fig. 6** ATR-IR spectra of membrane surface during UV cleaning in case of oil-in-water emulsion with no added salt (**a, d**) and with 250 mg L<sup>-1</sup> (**b, e**) and 2500 mg L<sup>-1</sup> added salt (**c, f**)

slightly increased irreversible (non-washable) resistances were observed, which can be explained by the DLVO theory, as increase in ionic strength lowers the energy barrier and hence favors adhesion. Cleaning the membrane with heterogeneous photocatalysis irradiating UVa significant flux recovery can be achieved, but the membrane surface wettability and ATR-IR measurements showed that the recovery of flux does not mean the total elimination of the oil layer from the membrane surface; however, the well-soluble oxidation by-products (e.g., small acids) cannot remain on the surface.

**Funding information** This project was supported by the János Bolyai Research Scholarship of the Hungarian Academy of Sciences. The authors received financial support from the project Hungarian Scientific Research Fund (NKFI contract number K112096).

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